

Optical Bragg Accelerators

Amit Mizrahi

Supervised by Prof. Levi Schächter



Technion – Israel Institute of Technology

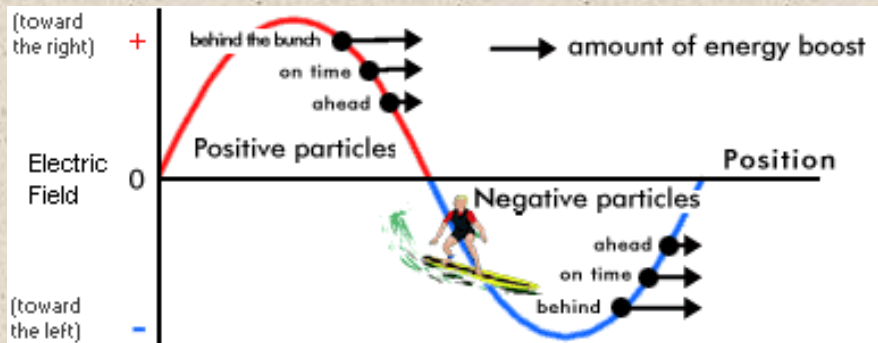
Department of Electrical Engineering

Outline

- Background
- Motivation
- Field Confinement
- Accelerator parameters
- Wake-field analysis
- Summary

How Do Accelerators Work?

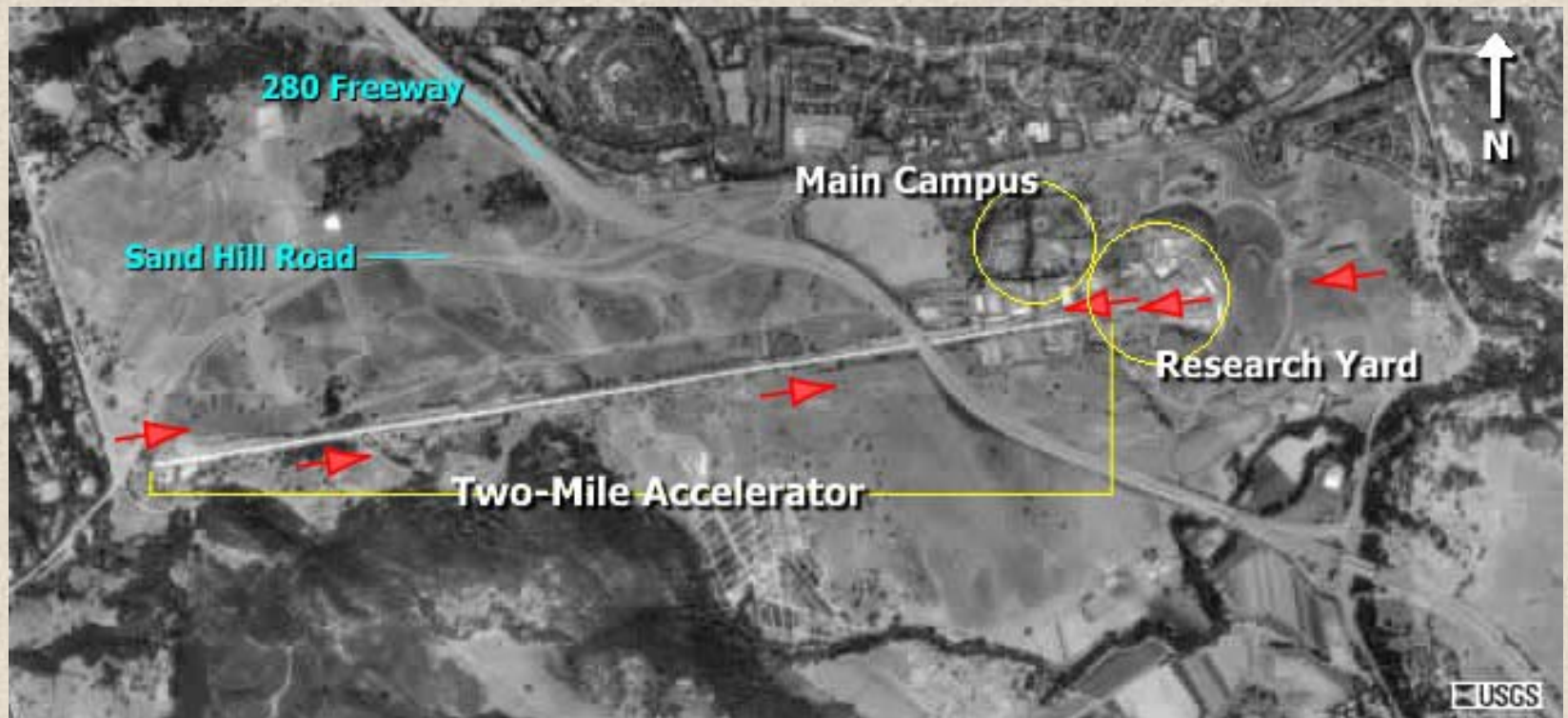
Charges “surf” on the longitudinal electric field



Phase velocity equals the speed of light!



Stanford Linear Accelerator



Motivation

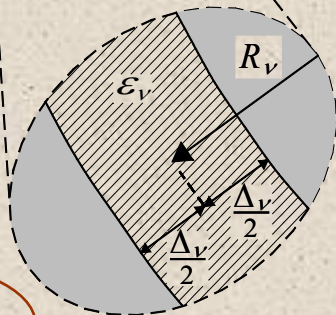
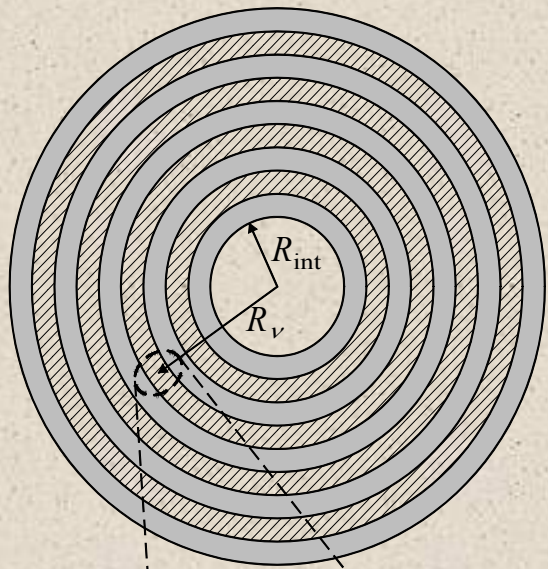
- Smaller and cheaper accelerators (table-top).
- Applications: X-ray, medical, materials.
- Availability of high power lasers.
- Dielectric materials can sustain higher fields than metals.
- Fabrication: harness communication technology.
- Need vacuum tunnel – confinement can not be achieved as in optical fibers – **Bragg waveguide!**

Objectives

Is a dielectric optical Bragg waveguide adequate for acceleration?

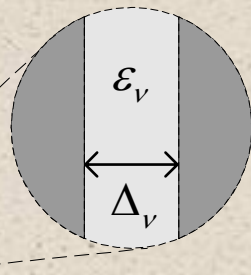
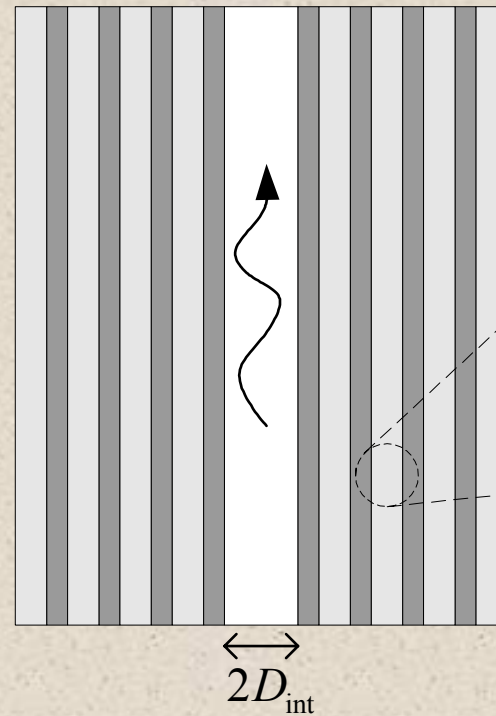
- Design of Bragg waveguide that supports propagation with phase velocity c for the driving laser frequency.
- Analyze accelerator parameters (interaction impedance, energy velocity, maximal field).
- Analyze wake-field due to a train of micro-bunches.

Hollow Bragg Fiber



$$\partial/\partial\phi \equiv 0$$

Planar Bragg Waveguide



$$\partial/\partial y \equiv 0$$

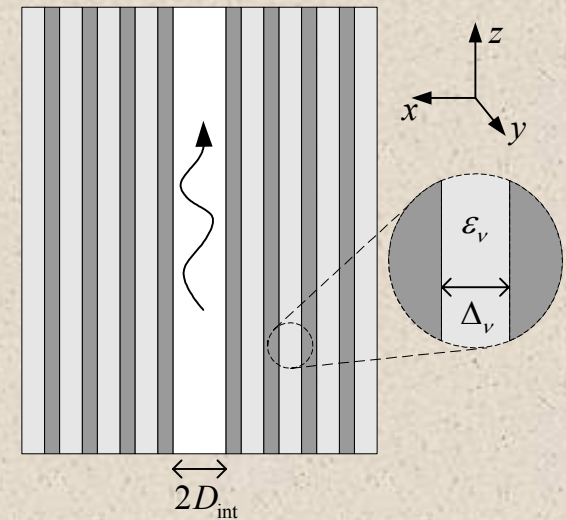
Required EM Fields

Vacuum fields

$$E_z = E_0 e^{-j\frac{\omega}{c}z}$$

$$E_x = j\frac{\omega}{c}xE_0 e^{-j\frac{\omega}{c}z}$$

$$H_y = \frac{j}{\eta_0}\frac{\omega}{c}xE_0 e^{-j\frac{\omega}{c}z}$$



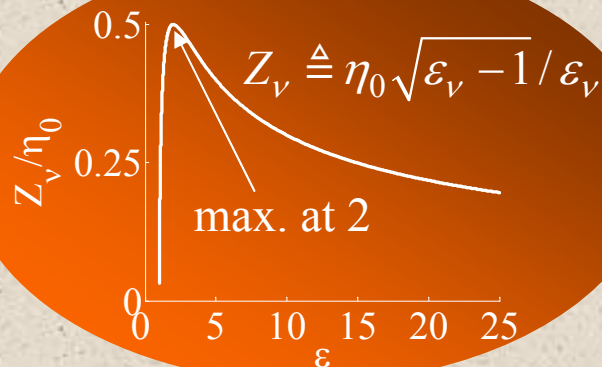
Fields in layer v

$$k_v \triangleq \frac{\omega}{c}\sqrt{\epsilon_v - 1}$$

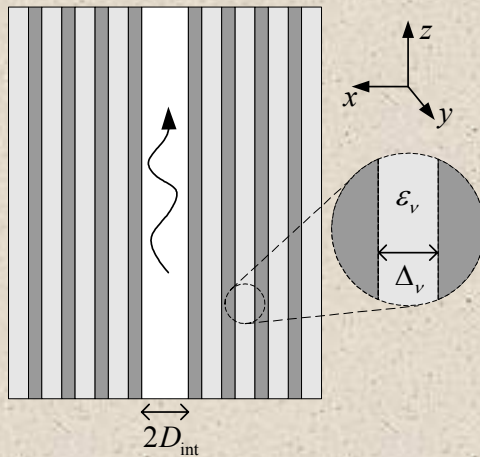
$$E_z = \left[A_v e^{-jk_v x} + B_v e^{+jk_v x} \right] e^{-j\frac{\omega}{c}z}$$

$$E_x = \frac{-1}{\sqrt{\epsilon_v - 1}} \left[A_v e^{-jk_v x} - B_v e^{+jk_v x} \right] e^{-j\frac{\omega}{c}z}$$

$$H_y = \frac{-1}{Z_v} \left[A_v e^{-jk_v x} - B_v e^{+jk_v x} \right] e^{-j\frac{\omega}{c}z}$$



Bragg Reflection



Application to Bragg waveguides

- Yeh *et al.*, Opt. Commun. **19**, 427–430, (1976).
- Yeh *et al.*, JOSA, **68**, 1196–1201, (1978).

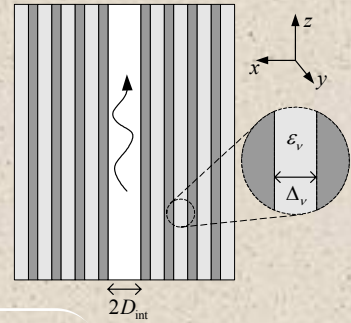
T – Unit cell Transition matrix of incoming and outgoing amplitudes of transverse waves

Eigen-value problem $|T - e^{-jKL}I| = 0$
L–periodicity, K–propagation coefficient

Dispersion relation $\cos(KL) = \frac{1}{2}(T_{11} + T_{22})$

Confinement condition $\left(\frac{T_{11} + T_{22}}{2}\right)^2 > 1$

Optimal Confinement



Confinement condition

$$\left(\frac{T_{11} + T_{22}}{2} \right)^2 = \left(\frac{(Z_1 + Z_2)^2}{4Z_1 Z_2} \cos(\chi_1 + \chi_2) - \frac{(Z_1 - Z_2)^2}{4Z_1 Z_2} \cos(\chi_1 - \chi_2) \right)^2$$



$$\left. \begin{array}{l} \chi_1 - \chi_2 = 0 \\ \chi_1 + \chi_2 = \pi \end{array} \right\} \Rightarrow \left| \frac{T_{11} + T_{22}}{2} \right|_{\max} = \frac{1}{2} \left(\frac{Z_1}{Z_2} + \frac{Z_2}{Z_1} \right)$$

$$\chi_{1,2} \triangleq 2\pi \frac{\Delta_{1,2}}{\lambda_0} \sqrt{\epsilon_{1,2} - 1}$$

Quarter λ structure !!

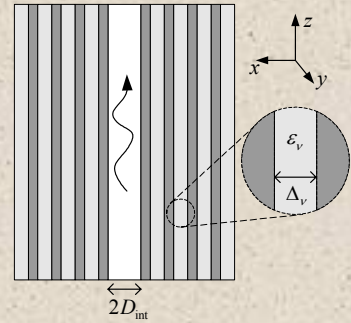


$$\chi_{1,2} = \frac{\pi}{2}$$



$$\Delta_{1,2} = \frac{\lambda_0}{4\sqrt{\epsilon_{1,2} - 1}}$$

Decay Coefficient



$$\cos(KL) = \frac{1}{2}(T_{11} + T_{22})$$

$$\left| \frac{T_{11} + T_{22}}{2} \right|_{\max} = \frac{1}{2} \left(\frac{Z_1}{Z_2} + \frac{Z_2}{Z_1} \right)$$



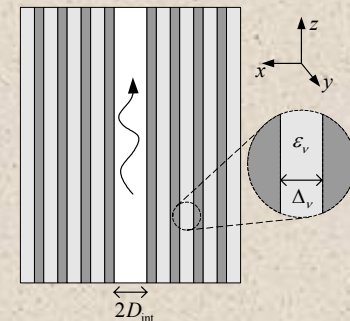
$$\left| e^{-jKL} \right|^n = \begin{cases} \left(\frac{Z_1}{Z_2} \right)^n & Z_1 < Z_2 \\ \left(\frac{Z_2}{Z_1} \right)^n & Z_1 > Z_2 \end{cases}$$

$$\left. \begin{matrix} Z_1 > Z_2 \\ x \simeq nL \end{matrix} \right\} \Rightarrow \left(\frac{Z_2}{Z_1} \right)^{2n} \simeq \left(\frac{Z_2}{Z_1} \right)^{2x/L} \triangleq \exp \left(-2 \frac{x}{x_c} \right)$$

Given subsequently

$$x_c = \frac{\lambda_0}{4} \left(\frac{1}{\sqrt{\epsilon_1 - 1}} + \frac{1}{\sqrt{\epsilon_2 - 1}} \right) \left| \ln^{-1} \left(\frac{\epsilon_1 \sqrt{\epsilon_2 - 1}}{\epsilon_2 \sqrt{\epsilon_1 - 1}} \right) \right|$$

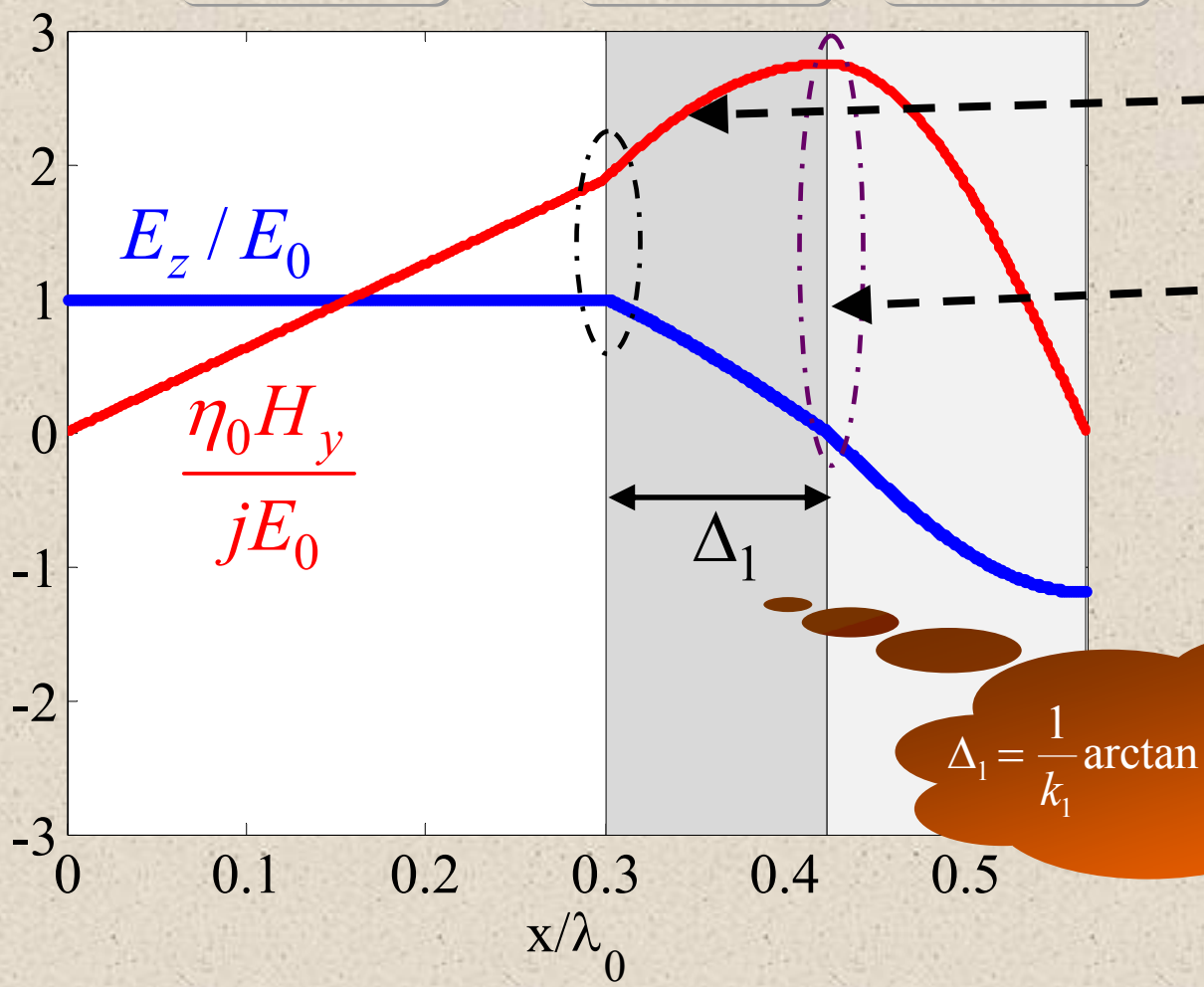
Field Confinement



vacuum

1st layer

2nd layer

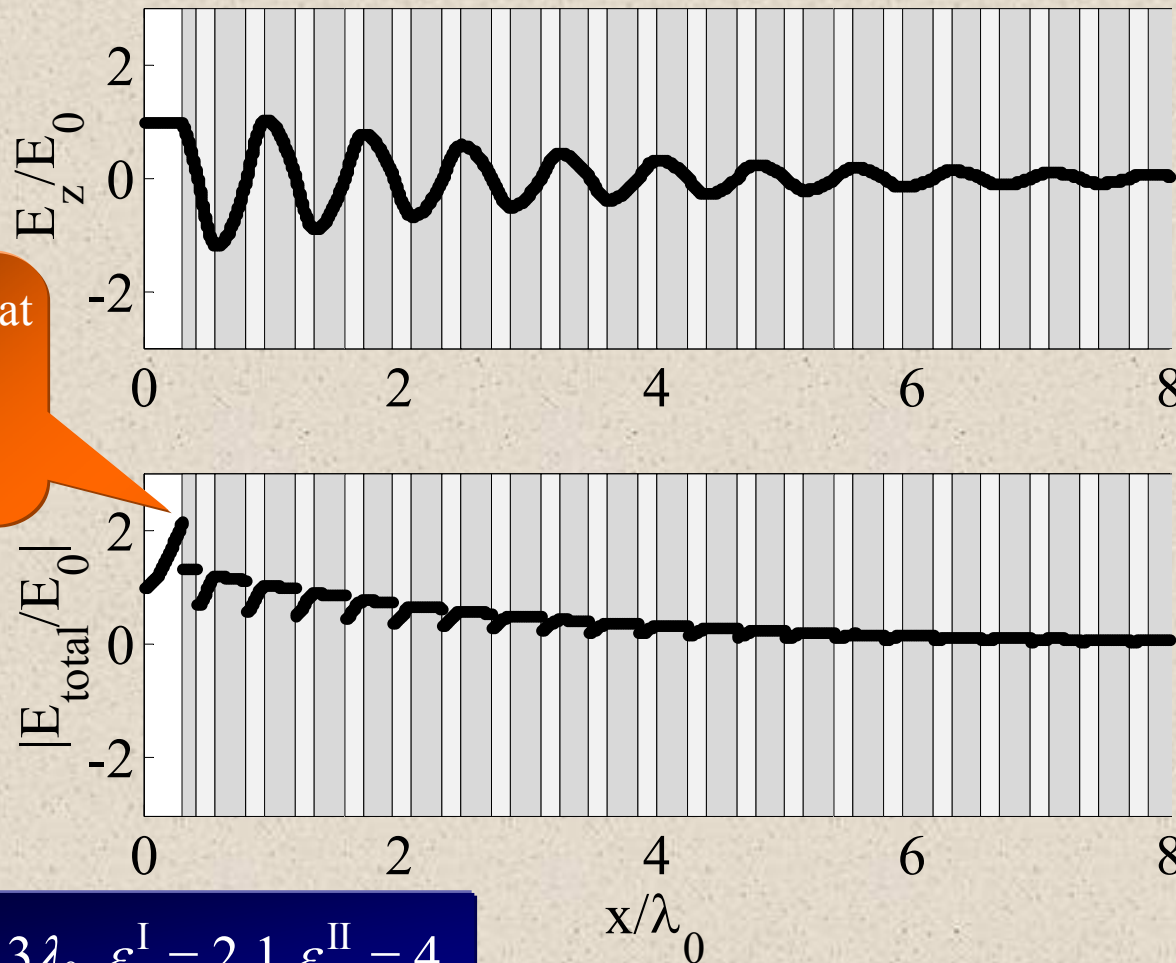
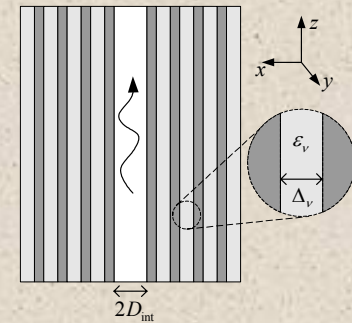


Dictated by vacuum fields.

Perfect reflection condition.

$$\Delta_1 = \frac{1}{k_1} \arctan \left[\left(\frac{Z_1 \omega_0}{\eta_0 c} D_{\text{int}} \right)^{-1} \right] \quad (Z_1 > Z_2)$$

Field Confinement – E_z Profile

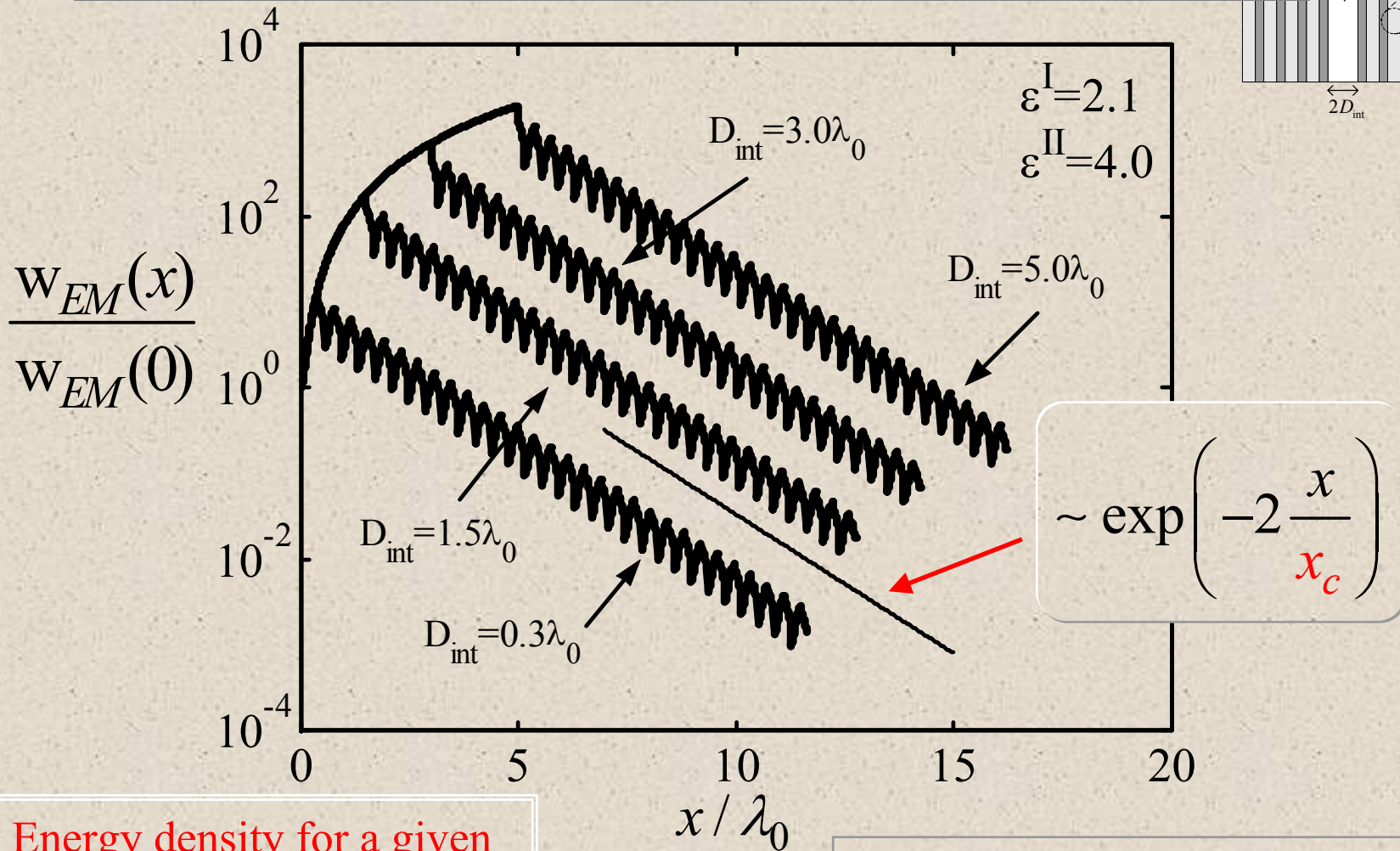
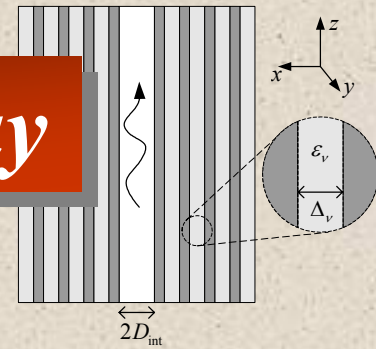


Maximum is at
vacuum-
dielectric
interface

E_z either peaks
or diminishes
at every
discontinuity

$$D_{\text{int}} = 0.3\lambda_0, \epsilon^{\text{I}} = 2.1, \epsilon^{\text{II}} = 4$$

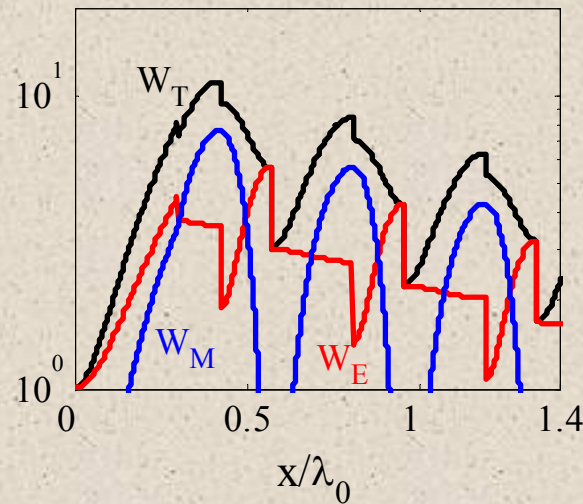
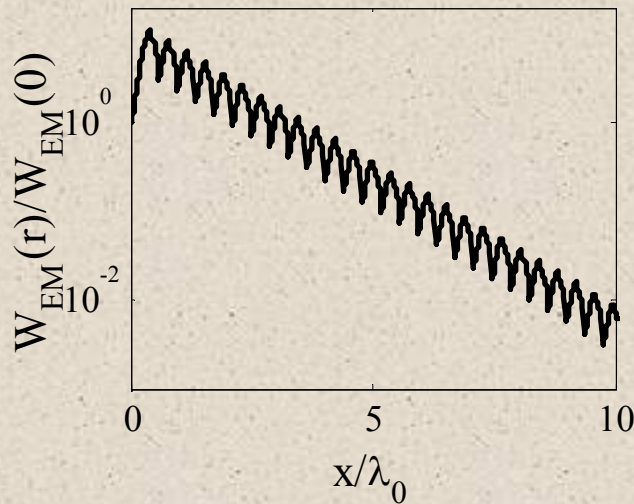
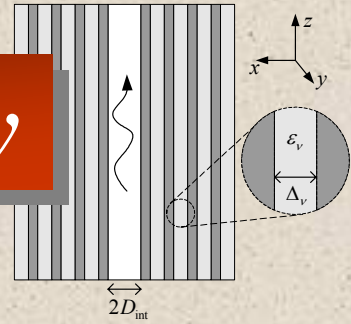
Field Confinement – Energy Decay



Energy density for a given E_0 increases for larger D_{int}/λ_0 !! Breakdown.

$$x_c = \frac{\lambda_0}{4} \left(\frac{1}{\sqrt{\epsilon_1 - 1}} + \frac{1}{\sqrt{\epsilon_2 - 1}} \right) \left| \ln^{-1} \left(\frac{\epsilon_1 \sqrt{\epsilon_2 - 1}}{\epsilon_2 \sqrt{\epsilon_1 - 1}} \right) \right|$$

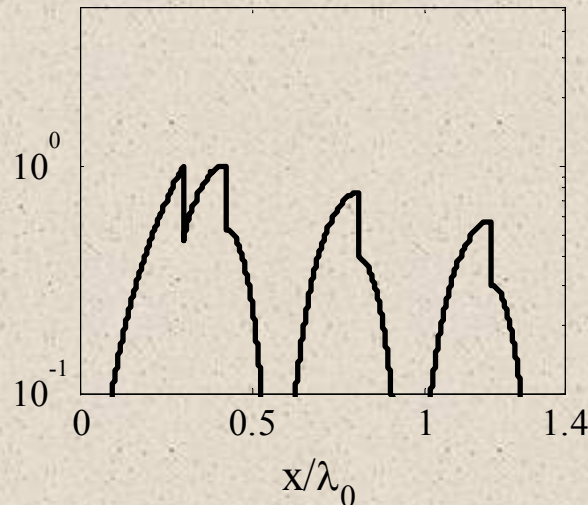
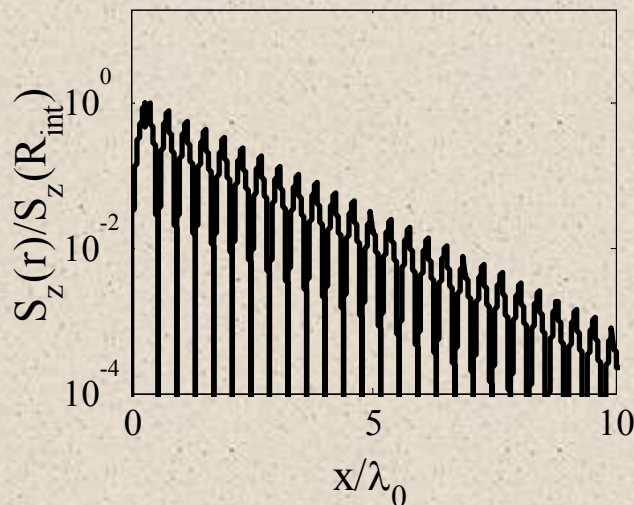
Field Confinement – Energy Decay



$$D_{\text{int}} = 0.3\lambda_0$$

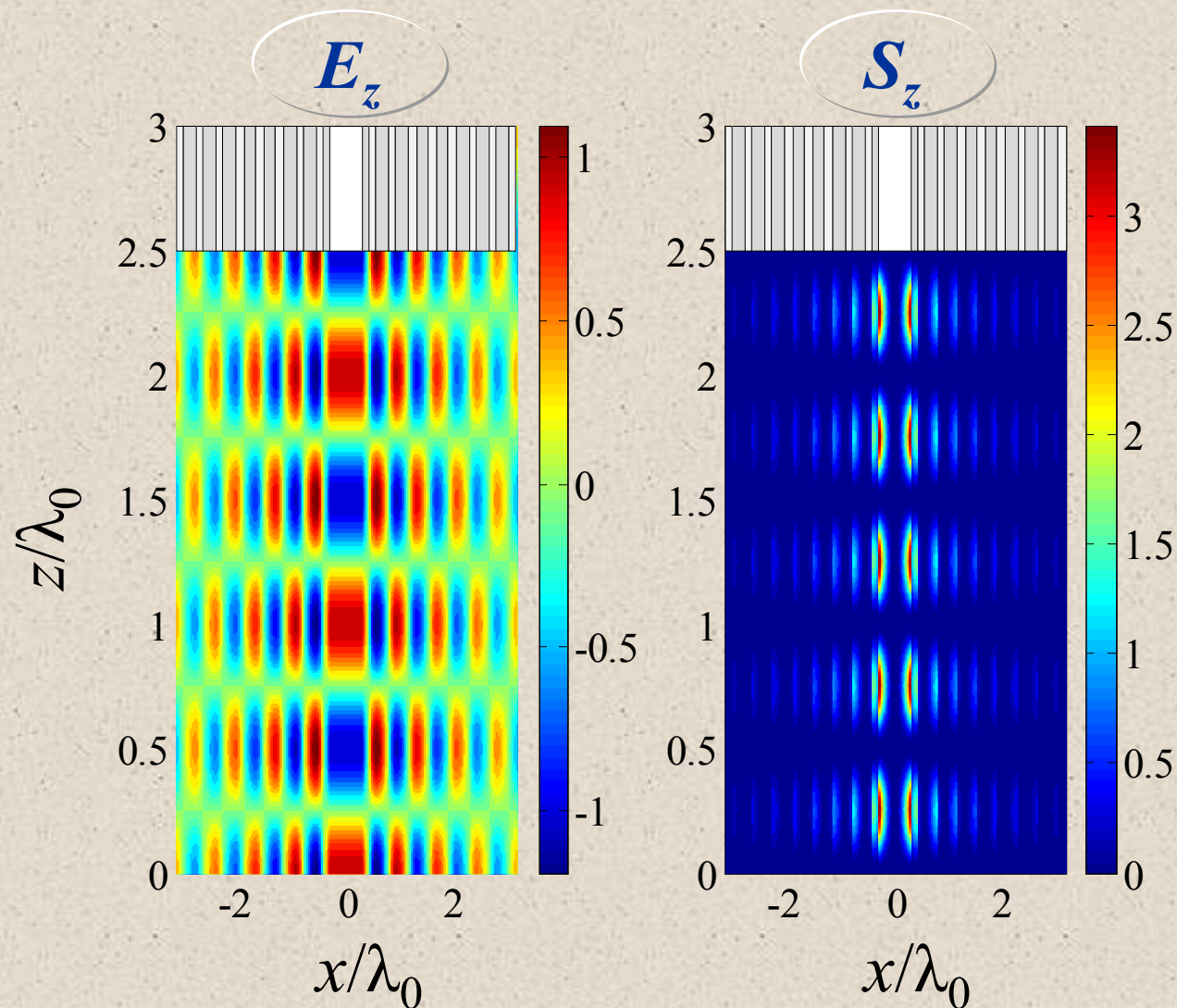
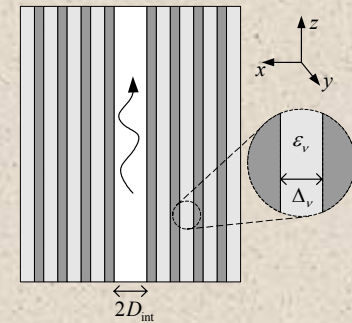
$$\varepsilon^{\text{I}} = 2.1$$

$$\varepsilon^{\text{II}} = 4$$



- Continuous W_M
- Discontinuous W_E
- W_M – zero-points
- E_z – zero-points
- S_z – zero-points

Field Confinement – $t=0$ Picture

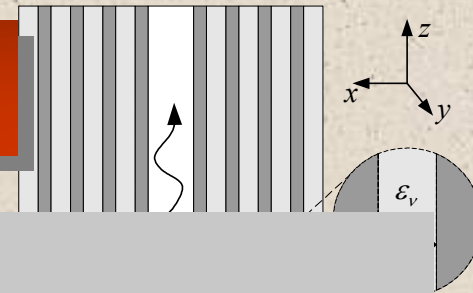


$$D_{\text{int}} = 0.3\lambda_0$$

$$\varepsilon^{\text{I}} = 2.1$$

$$\varepsilon^{\text{II}} = 4$$

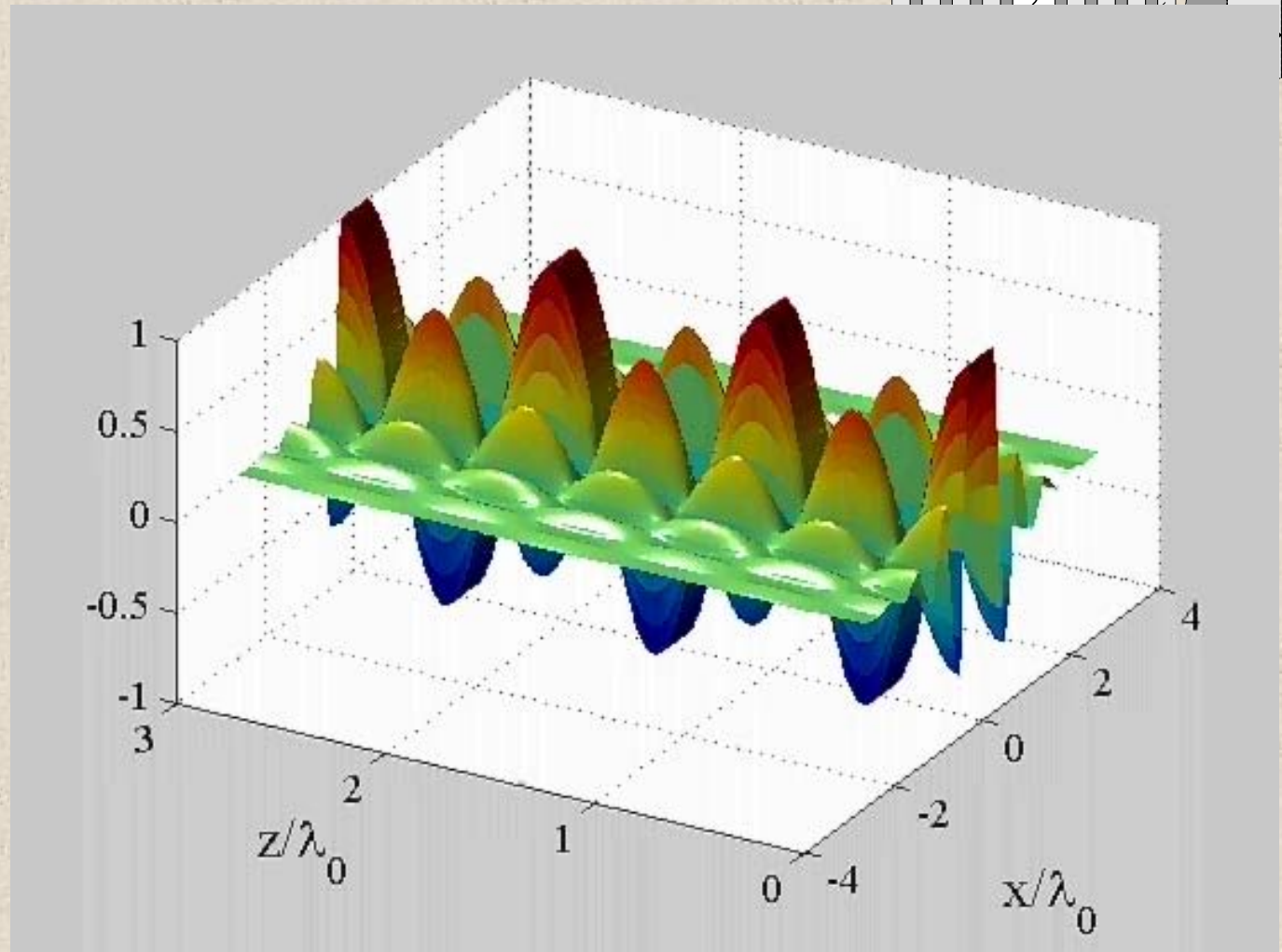
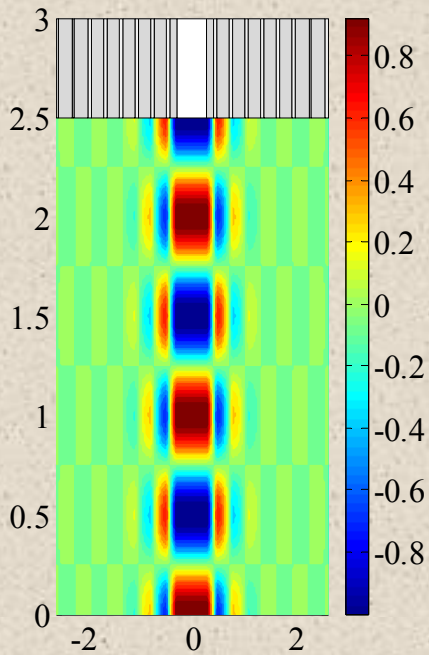
Field Confinement – The Movie



$$D_{\text{int}} = 0.3\lambda_0$$

$$\epsilon^{\text{I}} = 2.1$$

$$\epsilon^{\text{II}} = 16$$



Field Confinement – Cylindrical Case

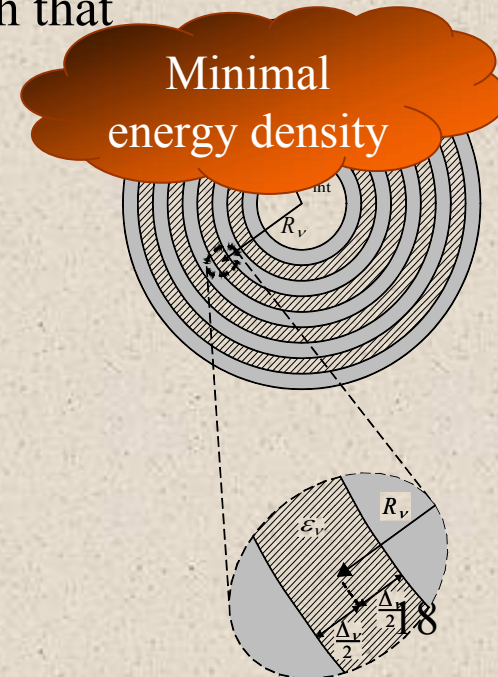
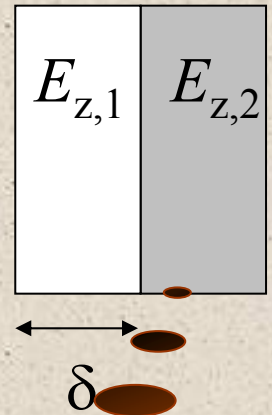
Generalization: if the impedance in the present layer is larger than in the next layer ($Z_1 > Z_2$), then the condition of minimum energy density is ensured provided the width of the present layer is chosen such that

$$E_{z,1}(\delta) = 0.$$

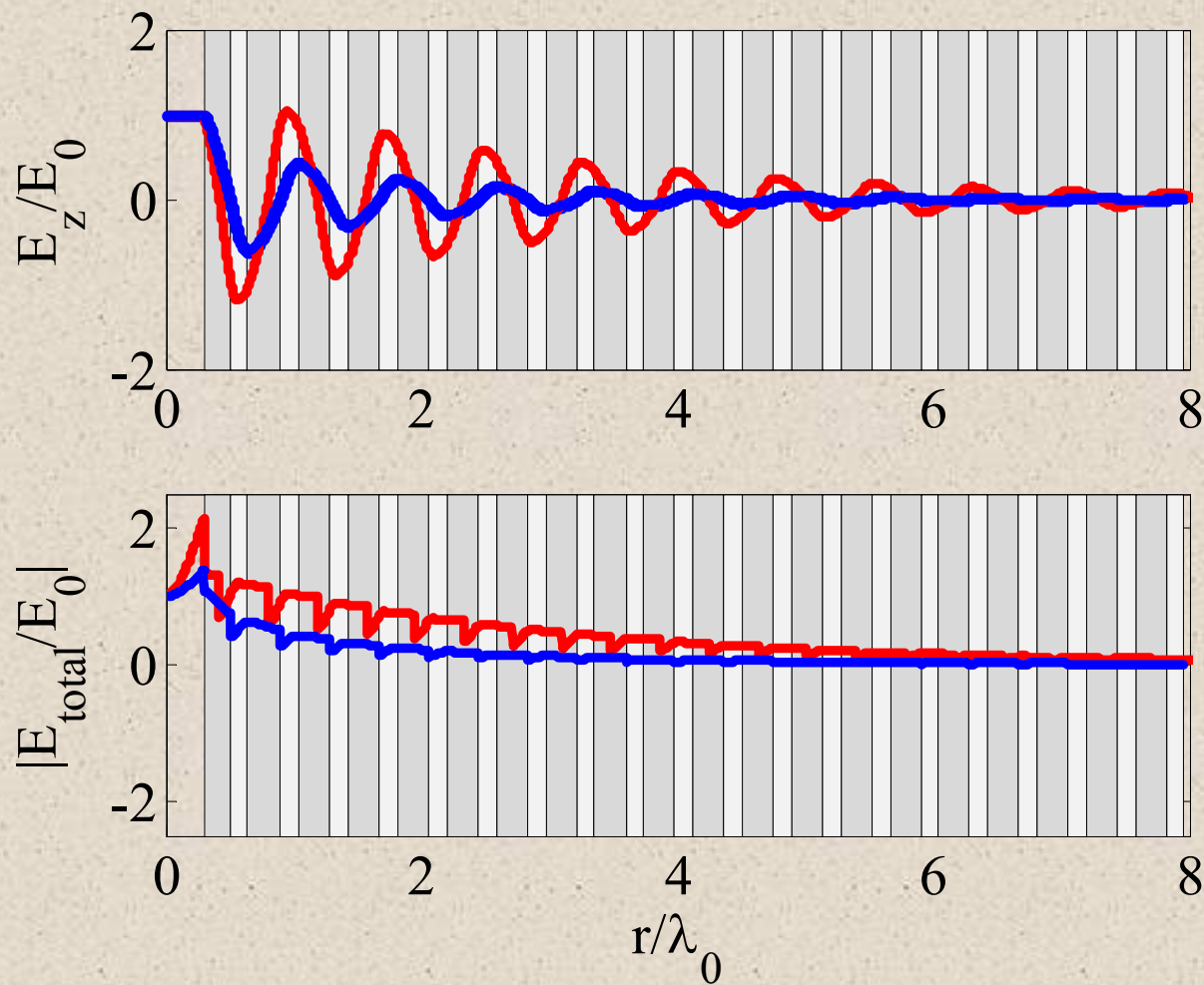
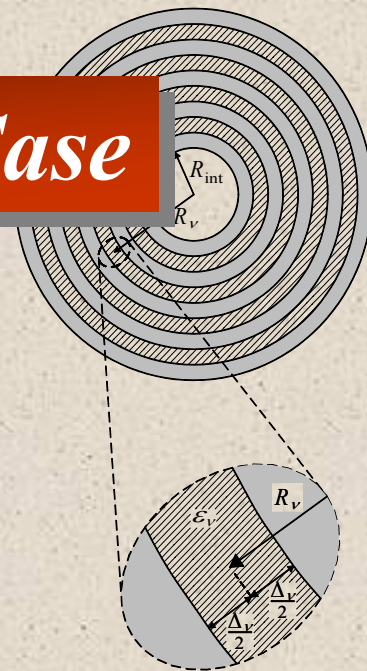
In a similar way, if the impedance in the present layer is smaller than in the next one ($Z_1 < Z_2$) then the width is determined such that the azimuthal magnetic field vanishes

$$\dot{E}_{z,1}(\delta) = 0$$

$$\begin{cases} E_{z,1}(\delta) = 0 & \text{if } Z_2 < Z_1 \\ \dot{E}_{z,1}(\delta) = 0 & \text{if } Z_2 > Z_1 \end{cases}$$



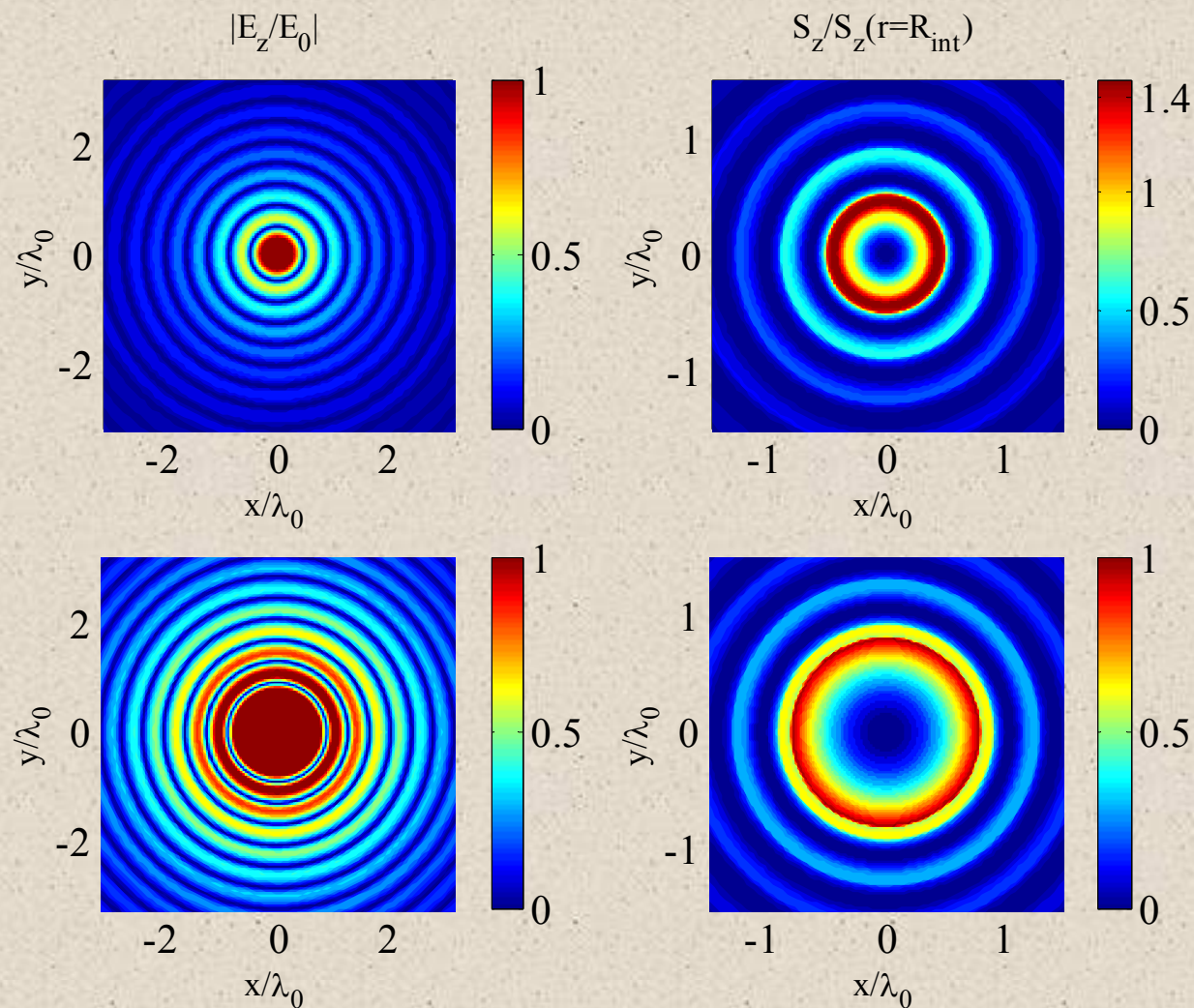
Field Confinement – Cylindrical Case



— cylindrical
— planar

$$\begin{aligned} R_{\text{int}} &= 0.3\lambda_0 \\ \epsilon^{\text{I}} &= 2.1 \\ \epsilon^{\text{II}} &= 4 \end{aligned}$$

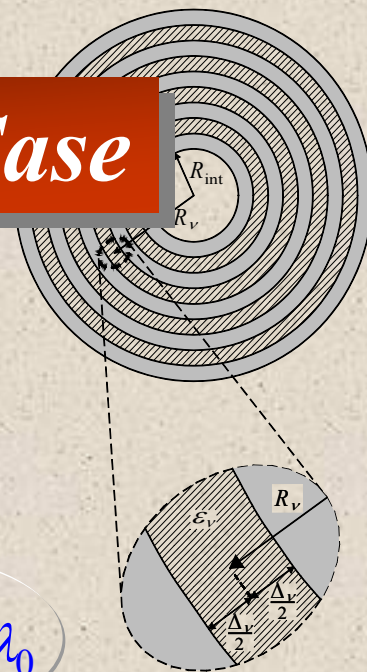
Field Confinement – Cylindrical Case



$$R_{\text{int}} = 0.3\lambda_0$$

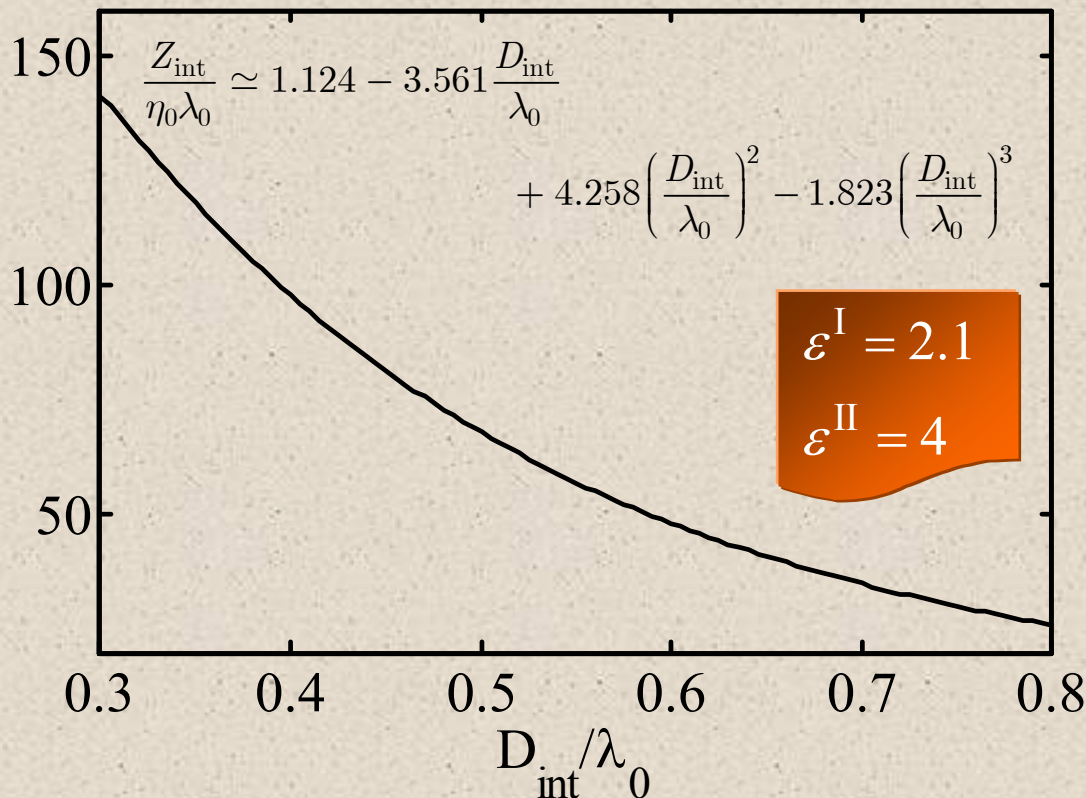
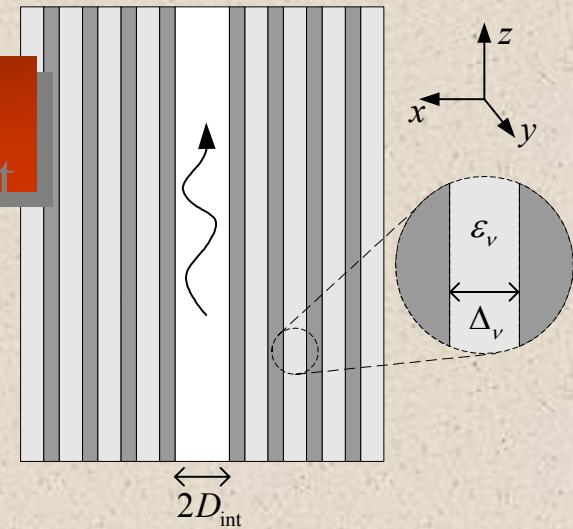
$$\begin{aligned}\varepsilon^{\text{I}} &= 2.1 \\ \varepsilon^{\text{II}} &= 4\end{aligned}$$

$$R_{\text{int}} = 0.8\lambda_0$$



Accelerator Parameters – Z_{int}

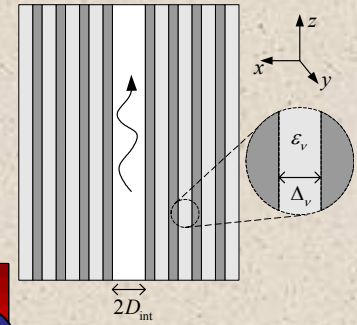
A measure for the amount of power flowing in the system for a given accelerating field.



$$Z_{\text{int}} [\Omega m] \triangleq \frac{(\lambda_0 E_0)^2}{P}$$

$$P \triangleq \int_{-\infty}^{\infty} dx S_z(x)$$

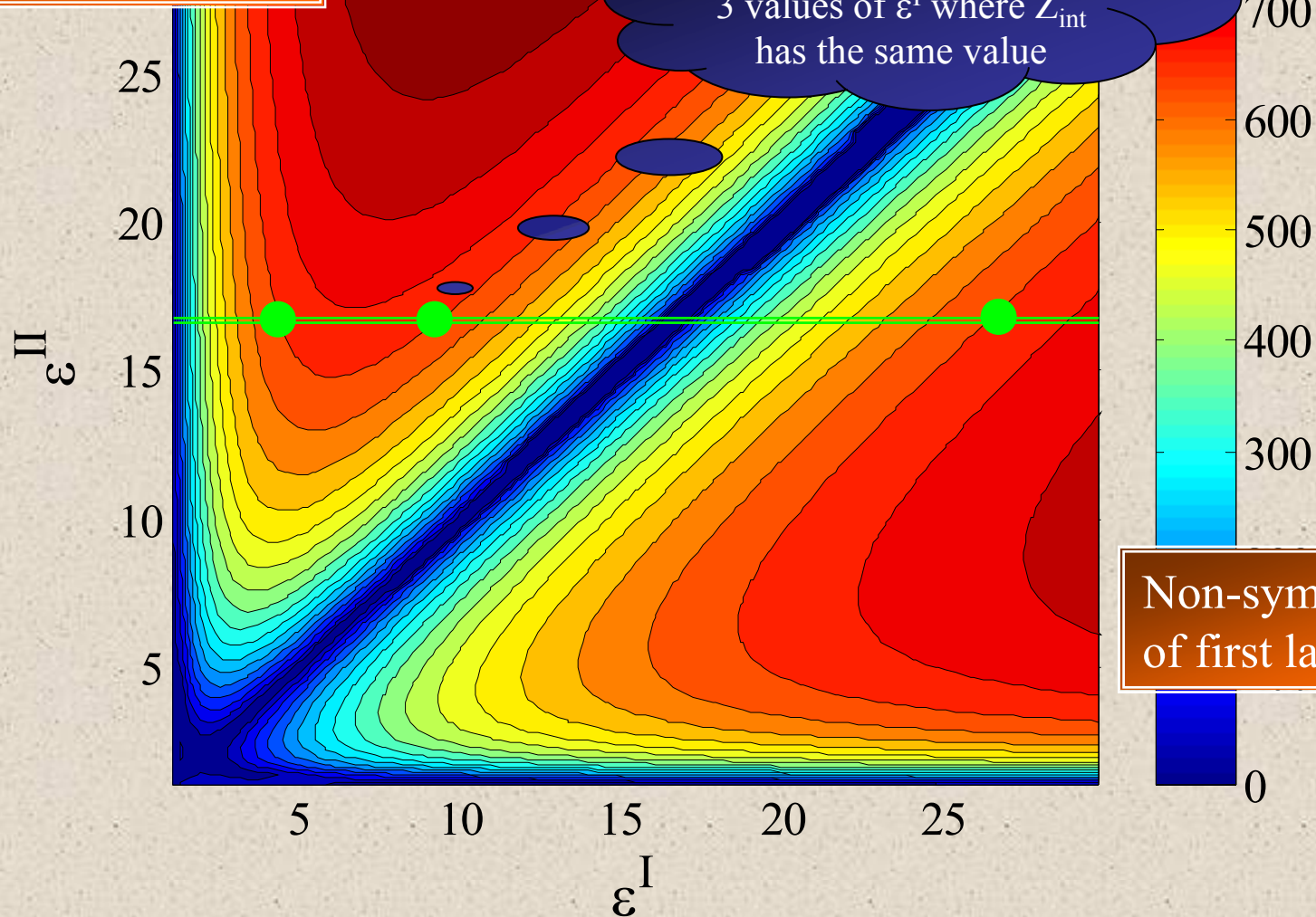
Accelerator Parameters – Z_{int}



High Z_{int} for large ε

For a given ε^{II} there are 3 values of ε^{I} where Z_{int} has the same value

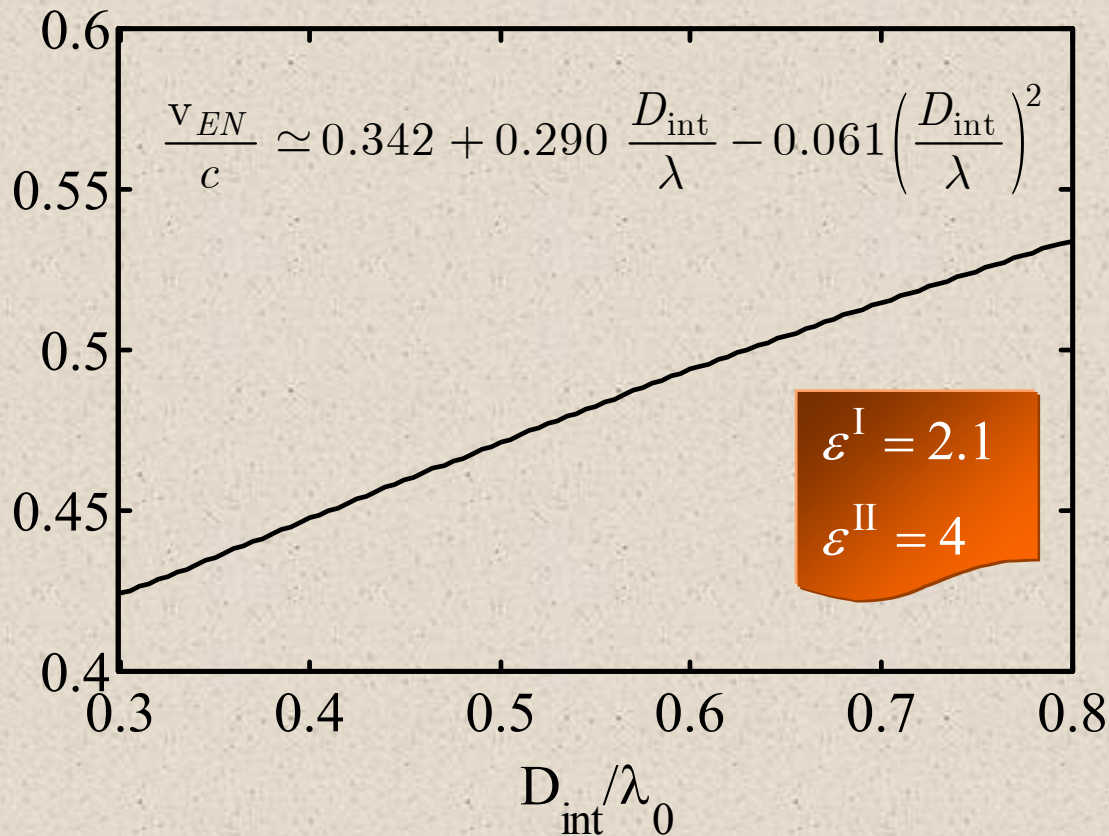
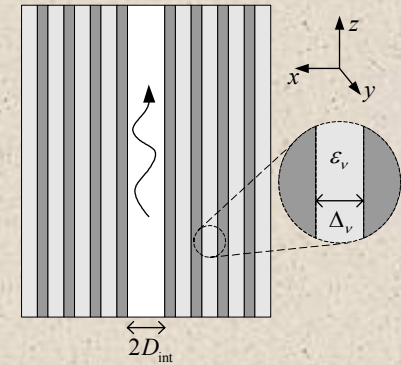
$$D_{\text{int}} = 0.3\lambda_0$$



Non-symmetry: role of first layer

Accelerator Parameters – v_{EN}

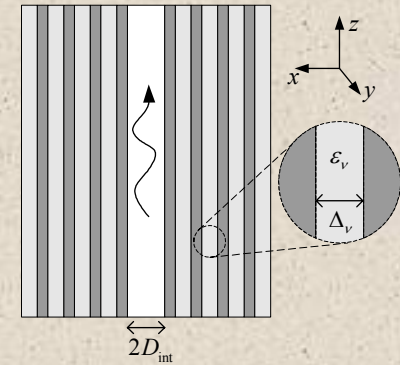
Equals the group velocity.



$$\frac{v_{EN}}{c} \triangleq \frac{P}{cW}$$

$$W \triangleq \int_{-\infty}^{\infty} dx w_{EM}(x)$$

Accelerator Parameters – $E_{\max}$



Planar

$$E_z = E_0 e^{-j\frac{\omega}{c}z}$$

$$E_x = j\frac{\omega}{c}x E_0 e^{-j\frac{\omega}{c}z}$$



$$\frac{E_{\max}}{E_0} = \sqrt{1 + \left(2\pi \frac{D_{\text{int}}}{\lambda_0}\right)^2}$$

$$2 \text{ [GV/m]}$$

$$\frac{E_{\max}}{E_0} = 2$$

$$1 \text{ [GV/m]}$$



$$D_{\text{int}} \simeq 0.28\lambda_0$$

$$R_{\text{int}} \simeq 0.55\lambda_0$$

Cylindrical

$$E_z = E_0 e^{-j\frac{\omega}{c}z}$$

$$E_r = j\frac{\omega}{c}\frac{1}{2}r E_0 e^{-j\frac{\omega}{c}z}$$

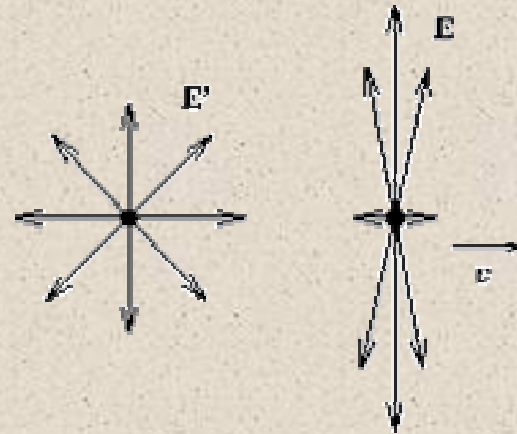


$$\frac{E_{\max}}{E_0} = \sqrt{1 + \left(\pi \frac{R_{\text{int}}}{\lambda_0}\right)^2}$$

Wake-Fields – Fields of Moving Charges

Charge in free space

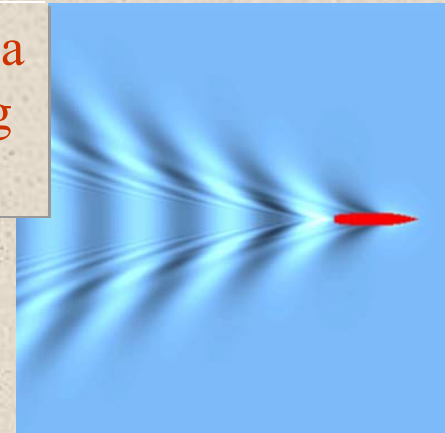
At high speed the field shrinks in the direction of motion.



Cerenkov radiation

A charge that exceeds the speed of light in the material (c/n) emits radiation.

Similarly to a ship moving in water

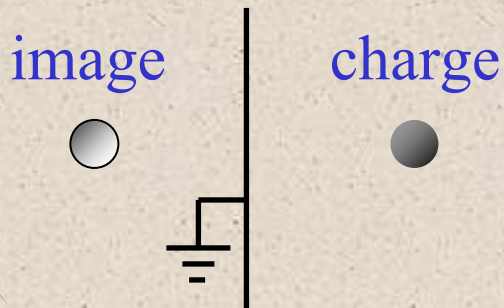


Wake-Field – General Approach

Primary field: free-space field of the moving charge.

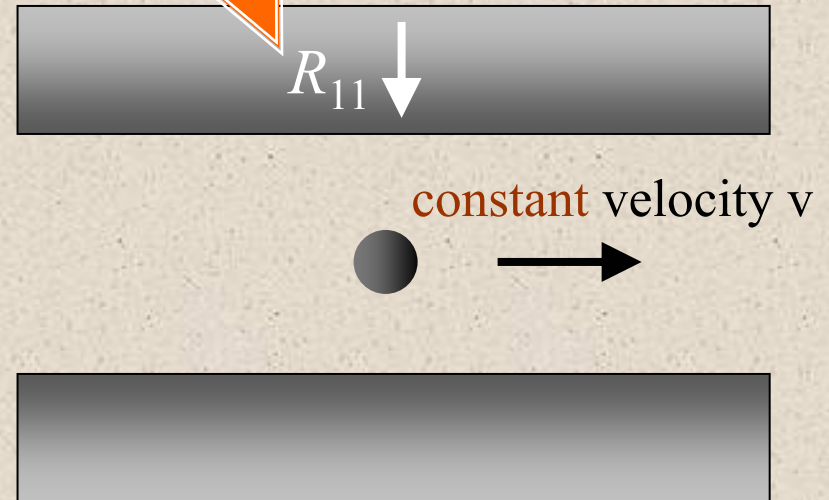
Secondary field: structure effect.

Static analogy



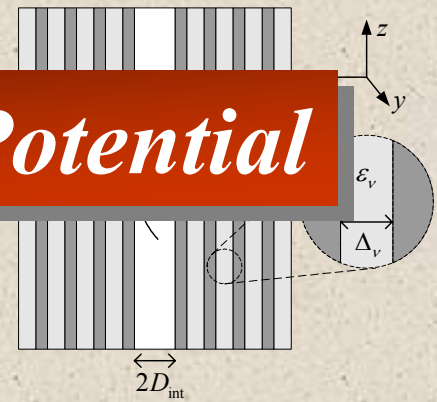
Reflection coefficient

Arbitrary structure



Schächter *et al.*, Phys. Rev. E, **68**, 036502 (2003).

Wake-Field – Magnetic Vector Potential



Moving line charge
 q – charge per unit length

$$J_z(x, z, t) = -q v \delta(x) \delta(z - vt)$$

Primary potential

$$A_z^{(p)}(x, z, t) = -\frac{q\mu_0}{4\pi} \int_{-\infty}^{\infty} d\omega e^{j\omega(t-z/v)} \frac{1}{\Gamma} e^{-\Gamma|x|}$$

$$\beta \triangleq v/c$$

$$\gamma \triangleq 1/\sqrt{1-v^2/c^2}$$

$$\Gamma \triangleq \frac{|\omega|}{c\gamma\beta}$$

$$\Lambda \triangleq \frac{|\omega|}{c} \sqrt{\epsilon_1 - \beta^{-2}}$$

Secondary potential

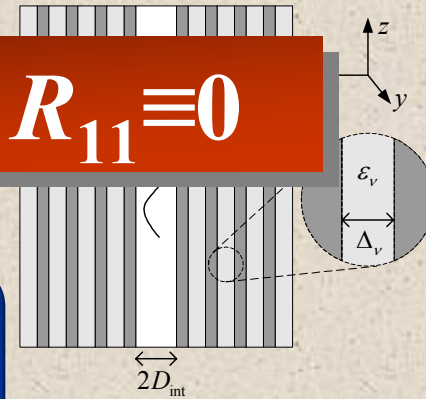
$$A_z^{(s)}(x, z, t) = -\frac{q\mu_0}{4\pi} \int_{-\infty}^{\infty} d\omega e^{j\omega(t-z/v)} \frac{1}{\Gamma} \begin{cases} B_0 \cosh(\Gamma x) & |x| < D_{\text{int}} \\ -\frac{\epsilon_1}{\gamma^2 \beta^2 (\epsilon_1 - \beta^{-2})} (C_0 e^{-j\Lambda x} + D_0 e^{j\Lambda x}) & x > D_{\text{int}} \end{cases}$$

All waves have $k_z = \omega/v$!!

$$R_{11} \triangleq \frac{D_0}{C_0} e^{2j\Lambda D_{\text{int}}}$$

Wake-Field – Decelerating Force $R_{11} \equiv 0$

$$E_{\parallel} \triangleq E_z^{(s)}(x=0, z=vt, t) = \frac{-q}{2\pi\epsilon_0 D_{\text{int}}} \text{Re} \left[j \ln \left(1 + j \frac{\gamma \sqrt{\beta^2 \epsilon_1 - 1}}{\epsilon_1} \right) \right]$$

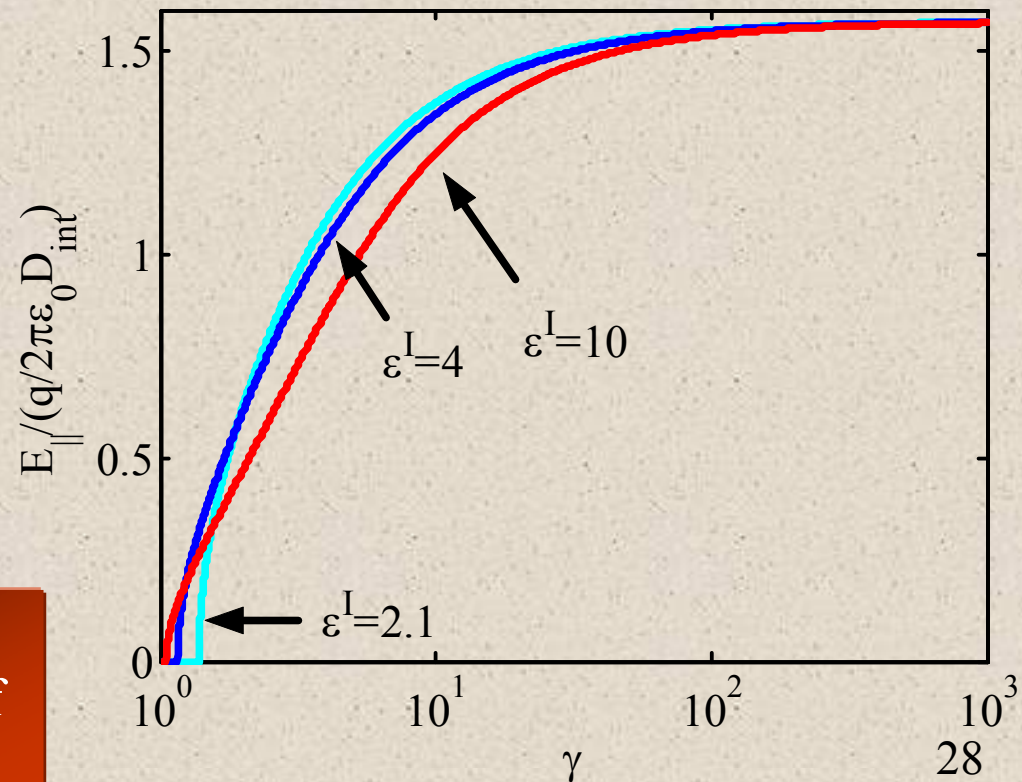


Ultra-relativistic regime $\gamma \rightarrow \infty$

$$E_{\parallel} = \frac{q}{2\pi\epsilon_0 D_{\text{int}}} \times \frac{\pi}{2}$$

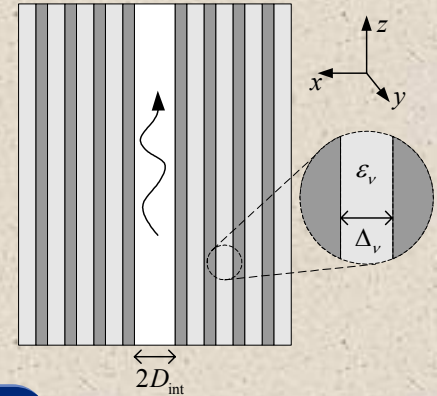
Static line-charge
field at D_{int}

In fact –
independent of
structure!!



Wake-Field On Axis

Ultra-relativistic wake-field on axis $\gamma \rightarrow \infty$

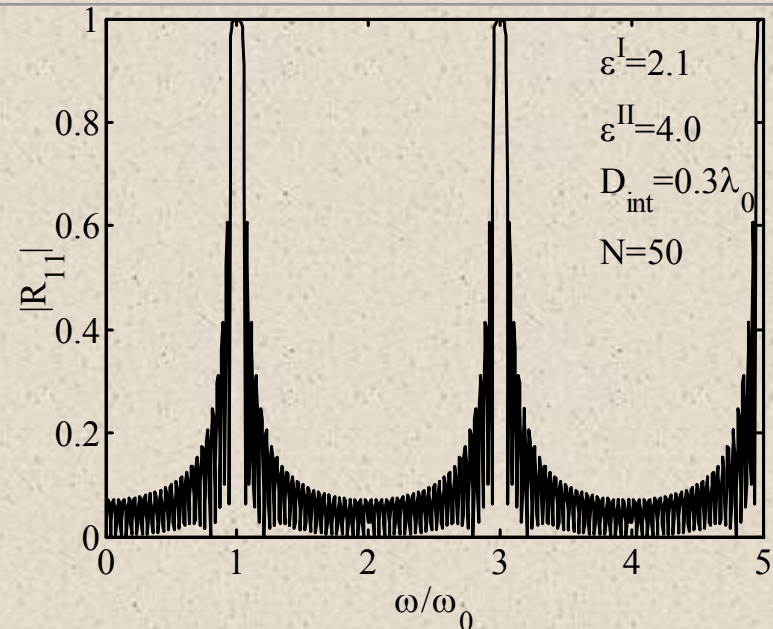


$$E_z^{(s)}(\bar{\tau}) = \frac{q}{2\pi\epsilon_0 D_{\text{int}}} \times \frac{1}{2} \int_{-\infty}^{\infty} d\bar{\omega} e^{j\bar{\omega}\bar{\tau}} \frac{1 + R_{11}(\bar{\omega})}{(1 + j\bar{\omega}) - (1 - j\bar{\omega})R_{11}(\bar{\omega})}$$

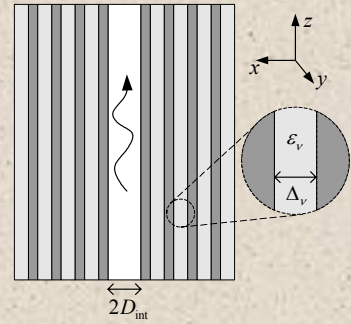
$$\bar{\omega} \triangleq \frac{\omega}{c} D_{\text{int}} \frac{\sqrt{\epsilon_1 - 1}}{\epsilon_1}$$

$$\bar{\tau} \triangleq \left(t - \frac{z}{c} \right) \frac{c}{D_{\text{int}}} \frac{\epsilon_1}{\sqrt{\epsilon_1 - 1}}$$

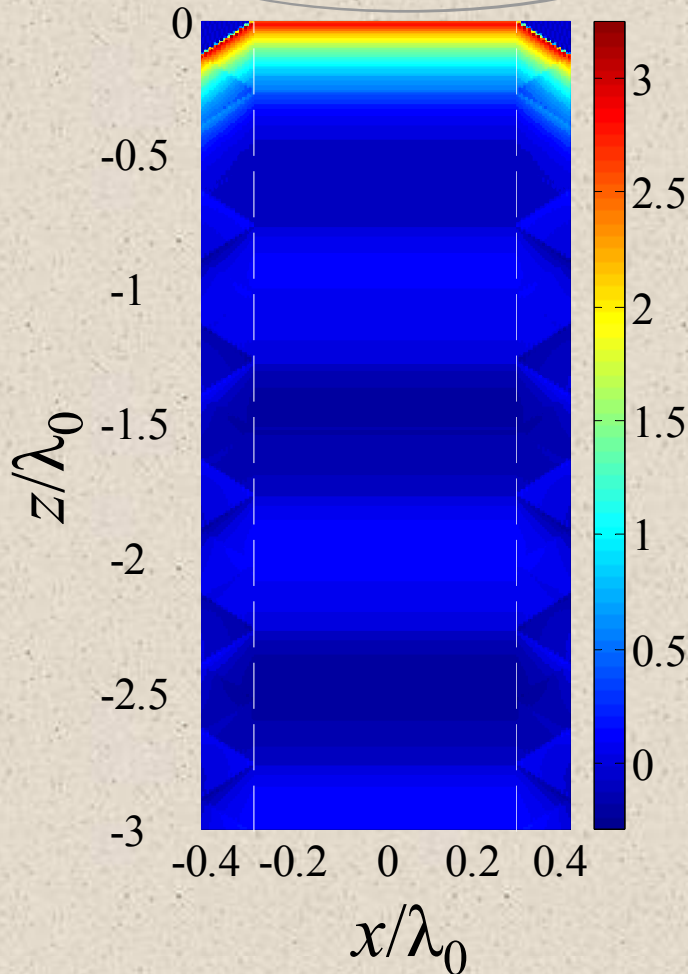
Reflection coefficient (analytic expression)



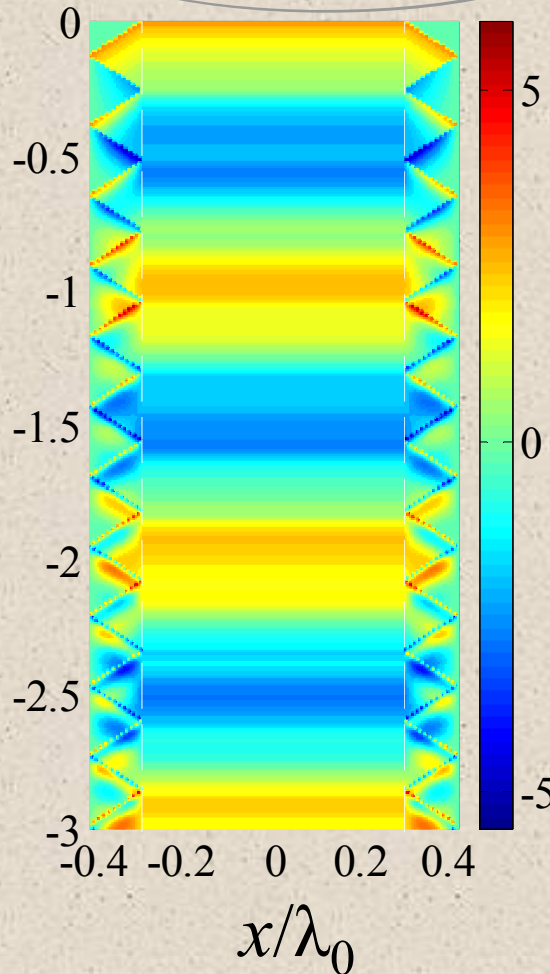
Wake-Field – $t=0$ Picture



Bragg Structure



Dielectric Loaded



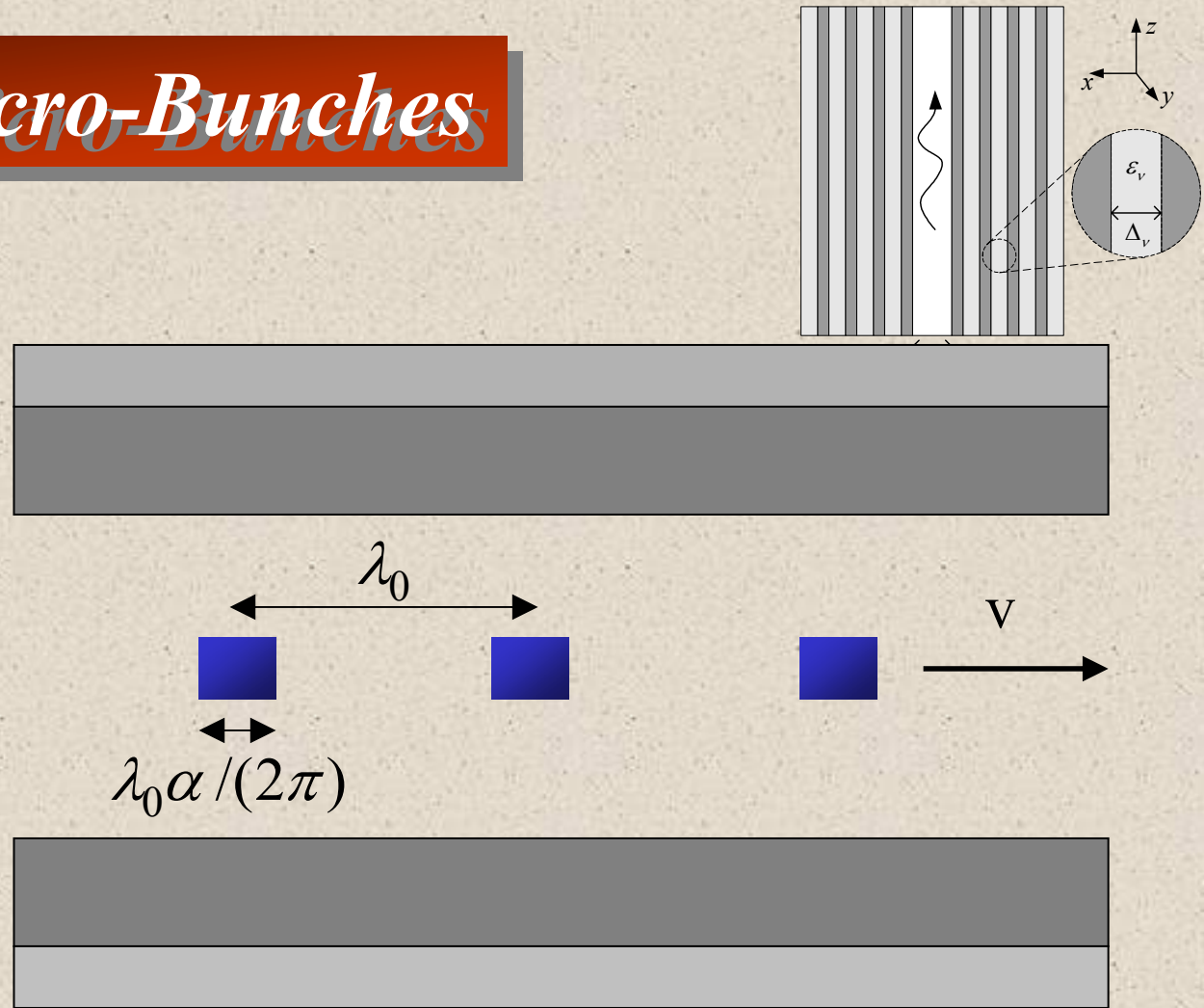
$$D_{\text{int}} = 0.3\lambda_0$$

$$\epsilon^{\text{I}} = 2.1$$

$$\epsilon^{\text{II}} = 4$$

Train of Micro-Bunches

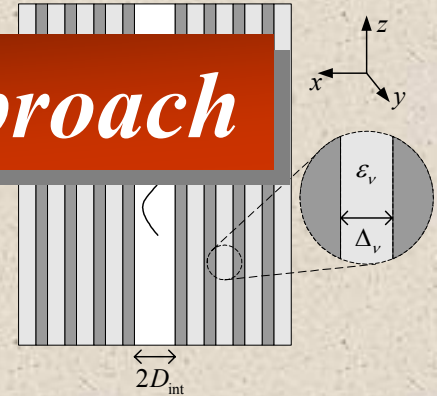
Total charge $-q$ is split into $M+1$ micro bunches.



Only secondary fields contribute to the emitted power.

Causality entails that each micro-bunch affects only the trailing micro-bunches.

Emitted Power – Qualitative Approach



one line-charge

$$P = \frac{vq^2}{2\pi\epsilon_0 D_{\text{int}}} \times \frac{\pi}{2}$$

Total power
neglecting
mutual effects.
 $q = N_{\text{el}} q_{\text{el}}, \alpha = 0$

$$P = \frac{vq_{\text{el}}^2 N_{\text{el}}^2 / (M+1)^2}{2\pi\epsilon_0 D_{\text{int}}} \times \frac{\pi}{2} \times (M+1) = \frac{vq_{\text{el}}^2}{2\pi\epsilon_0 D_{\text{int}}} \times \frac{N_{\text{el}}^2}{(M+1)} \times \frac{\pi}{2}$$

One micro-bunch
(line-charge)

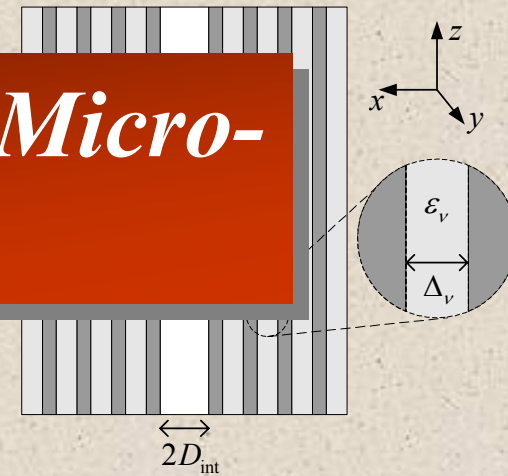
$$P = \frac{vq_{\text{el}}^2}{2\pi\epsilon_0 D_{\text{int}}} \times \frac{\pi}{2} \times N_{\text{el}}^2$$

$\sim 1/(M+1)$

Randomly
distributed

$$P = \frac{vq_{\text{el}}^2}{2\pi\epsilon_0 D_{\text{int}}} \times \frac{\pi}{2} \times N_{\text{el}}$$

Emitted Power from a Train of Micro-Bunches – Exact Expression



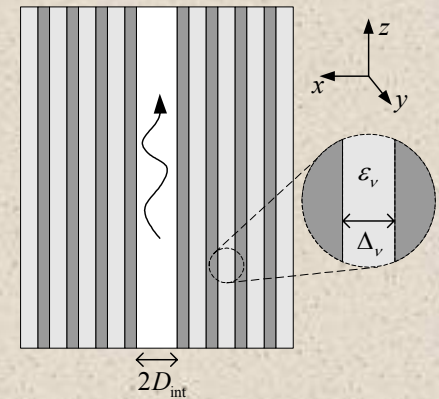
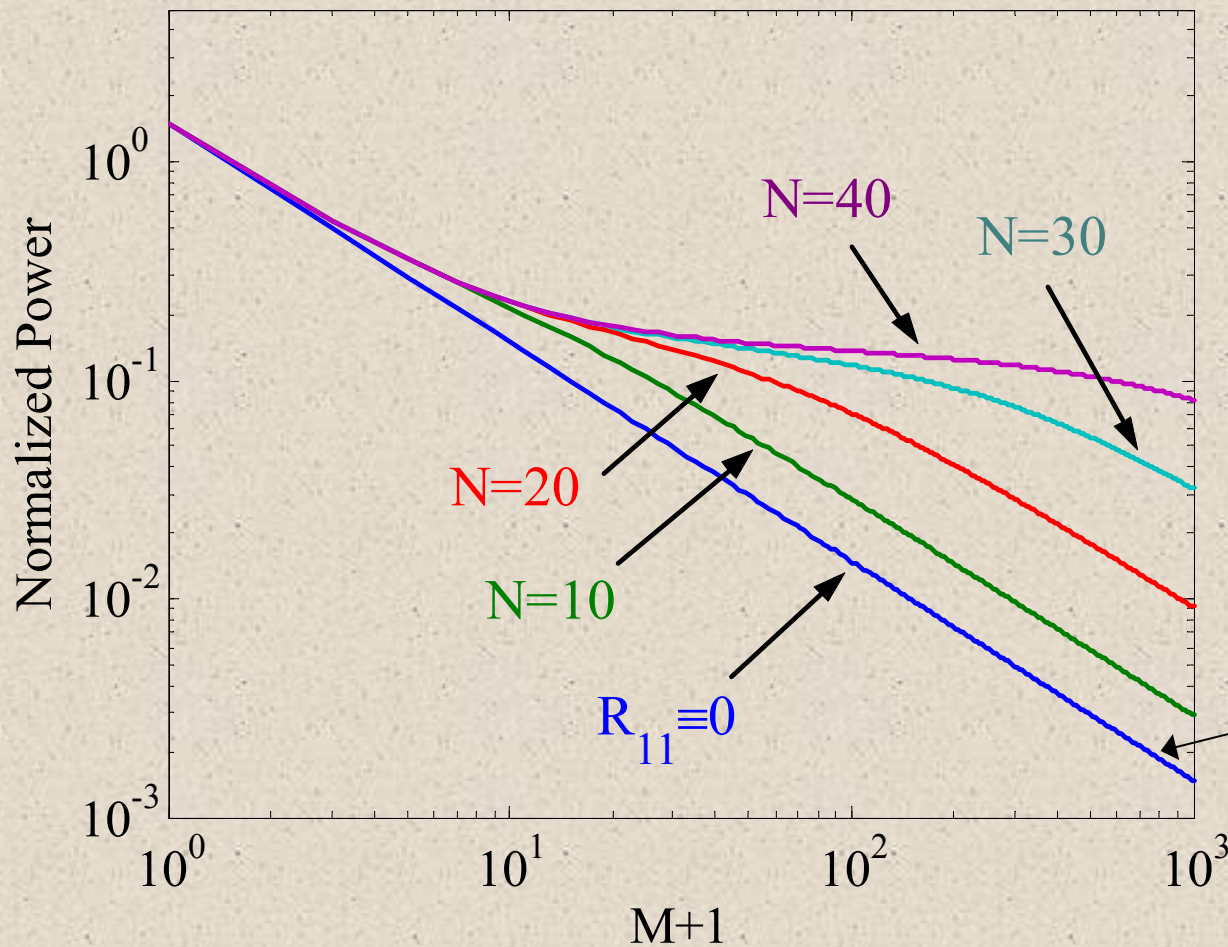
$$P = \frac{vq^2}{2\pi\epsilon_0 D_{\text{int}}} \frac{1}{2} \int_{-\infty}^{\infty} d\bar{\omega} \frac{1 + R_{11}(\bar{\omega})}{(1 + j\bar{\omega}) - (1 - j\bar{\omega})R_{11}(\bar{\omega})}$$

$$\times \text{sinc}^2 \left[\frac{\alpha}{2} \frac{\bar{\omega}}{\bar{\omega}_0} \right] \frac{\text{sinc}^2 \left[\pi \frac{\bar{\omega}}{\bar{\omega}_0} (M + 1) \right]}{\text{sinc}^2 \left[\pi \frac{\bar{\omega}}{\bar{\omega}_0} \right]}$$

Emitted Power

$$P = \frac{vq^2}{2\pi\epsilon_0 D_{\text{int}}} \frac{1}{2} \int_{-\infty}^{\infty} d\bar{\omega} \frac{1 + R_{11}(\bar{\omega})}{(1 + j\bar{\omega}) - (1 - j\bar{\omega})R_{11}(\bar{\omega})}$$

$$\times \text{sinc}^2 \left[\frac{\alpha}{2} \frac{\bar{\omega}}{\bar{\omega}_0} \right] \frac{\text{sinc}^2 \left[\pi \frac{\bar{\omega}}{\bar{\omega}_0} (M+1) \right]}{\text{sinc}^2 \left[\pi \frac{\bar{\omega}}{\bar{\omega}_0} \right]}$$



$\sim 1/(M+1)$

Summary

- Detailed design of Bragg acceleration structures – theoretical feasibility was shown!
- Structure parameters suitable for acceleration purposes (interaction impedance, energy velocity, maximal field).
- Interaction impedance over 10 times larger than that of PBG [Lin, Phys. Rev. STAB, 4, 051301 (2001)].
- Better materials can dramatically improve performance.
- Analysis of Wake-field – power decreases with the number of micro-bunches, and increases with the number of layers.